

# **Specifications For Building Instrumentation**



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## SMIP Specifications

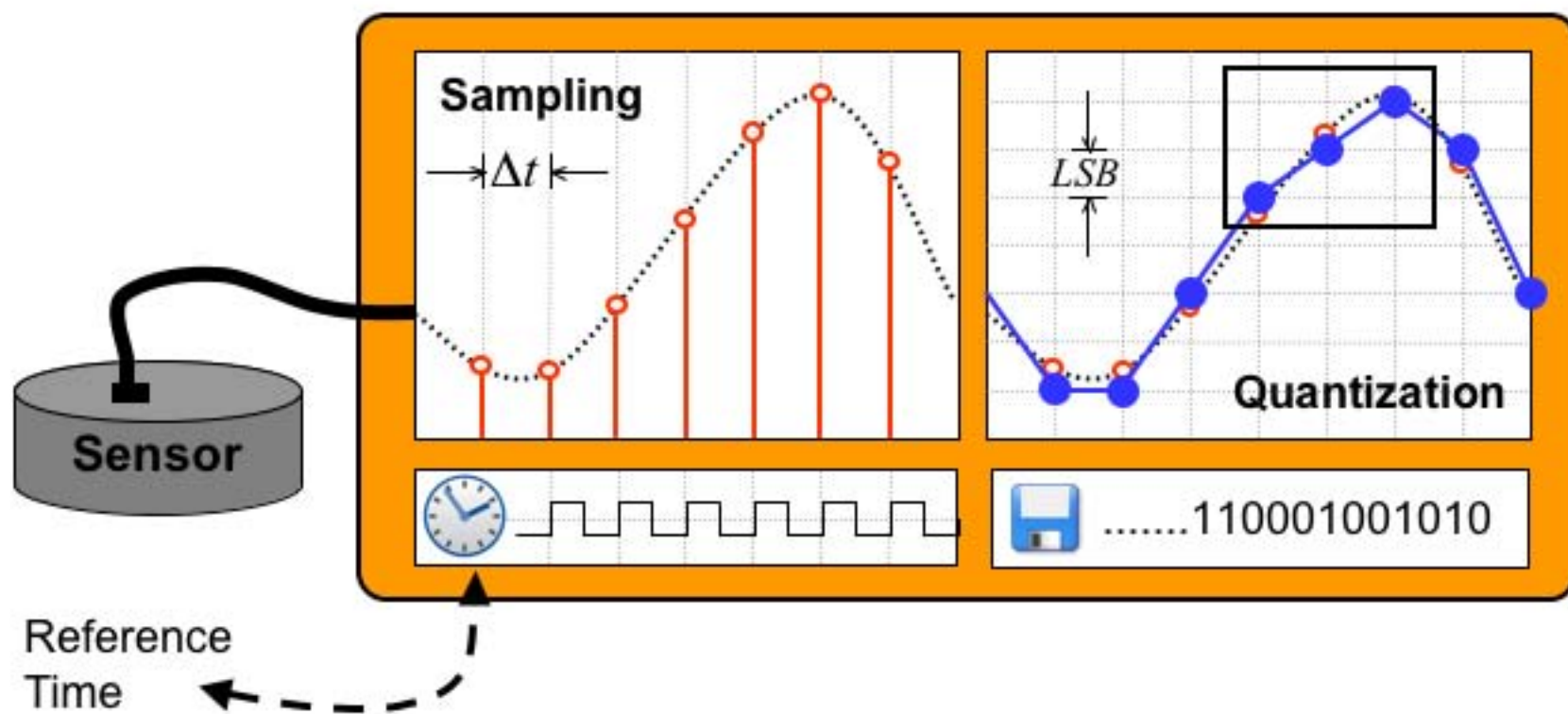
- Recommended specifications for civil structures (buildings)
- Based on qualitative assessment and experience

Recommended Specification	ANSS (USGS 2005)	CSMIP (CGS 2007)	
Sensor Range	±4g	± 4g	R (bits/g)
ADC Resolution	16bits	18bits	
Sample Rate	200sps	200sps	S (sps)
Sample Sync	1% $\Delta t$	0.2ms	$T_{se}$ (ms)
Reference Time	1.0ms	0.5ms	
Clock Stability	0.1ppm	1min/month	

*Guideline for ANSS Seismic Monitoring of Engineered Civil Systems, USGS Report 2005-1039  
Integrated Tri-Axial Accelerograph, CGS/DGS SYSREQ 2007-TR*

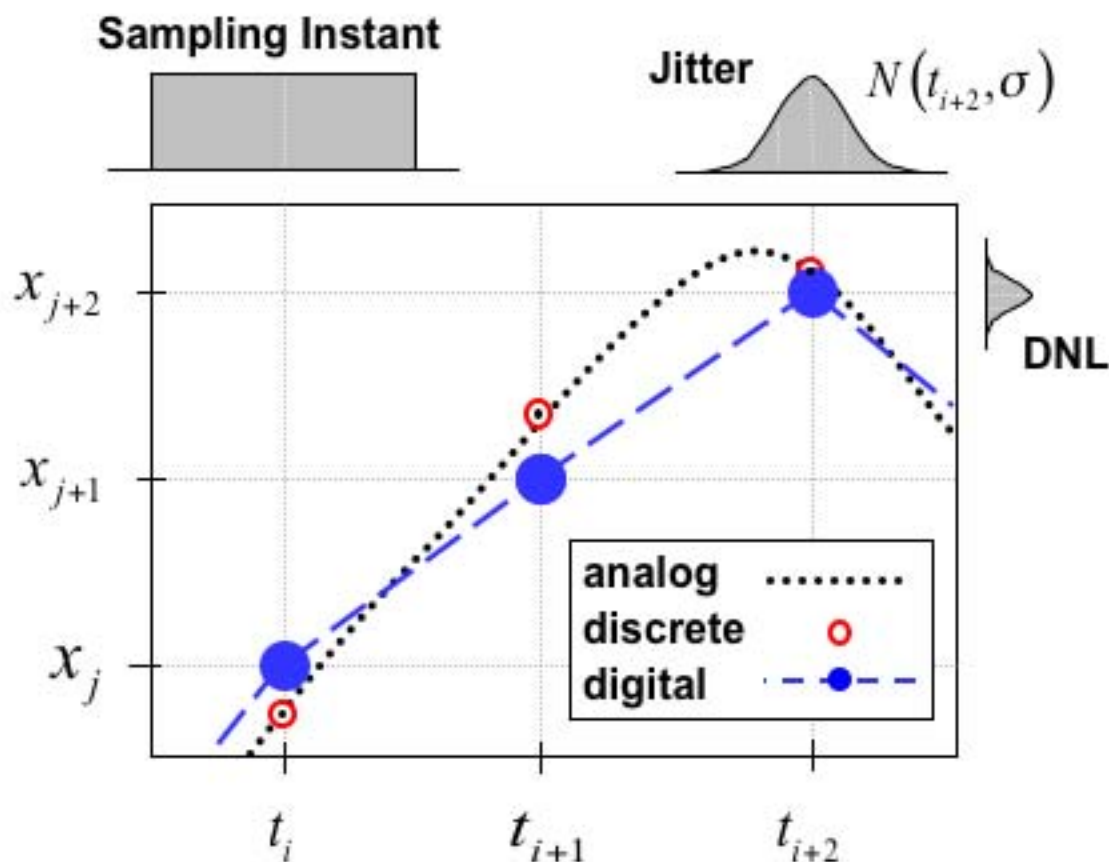
## Data Acquisition Systems (DAS)

- Sampling – sample rate ( $sps = 1 / \Delta t$ )
- Quantization – resolution ( $LSB = Range / 2^{Bits}$ )
- Time stamp for synchronization of multiple channels



## Data Acquisition Errors

- Sampling – initial sampling instant and clock jitter
- Quantization – Differential Non-Linearity (DNL)

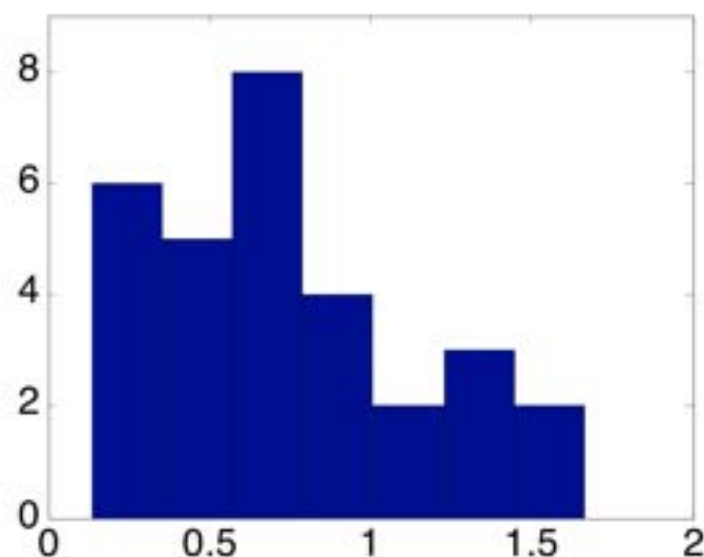


- Introduction
- DAS Specifications
- **DAQ Simulation**
- Sensitivity Studies
- Conclusions

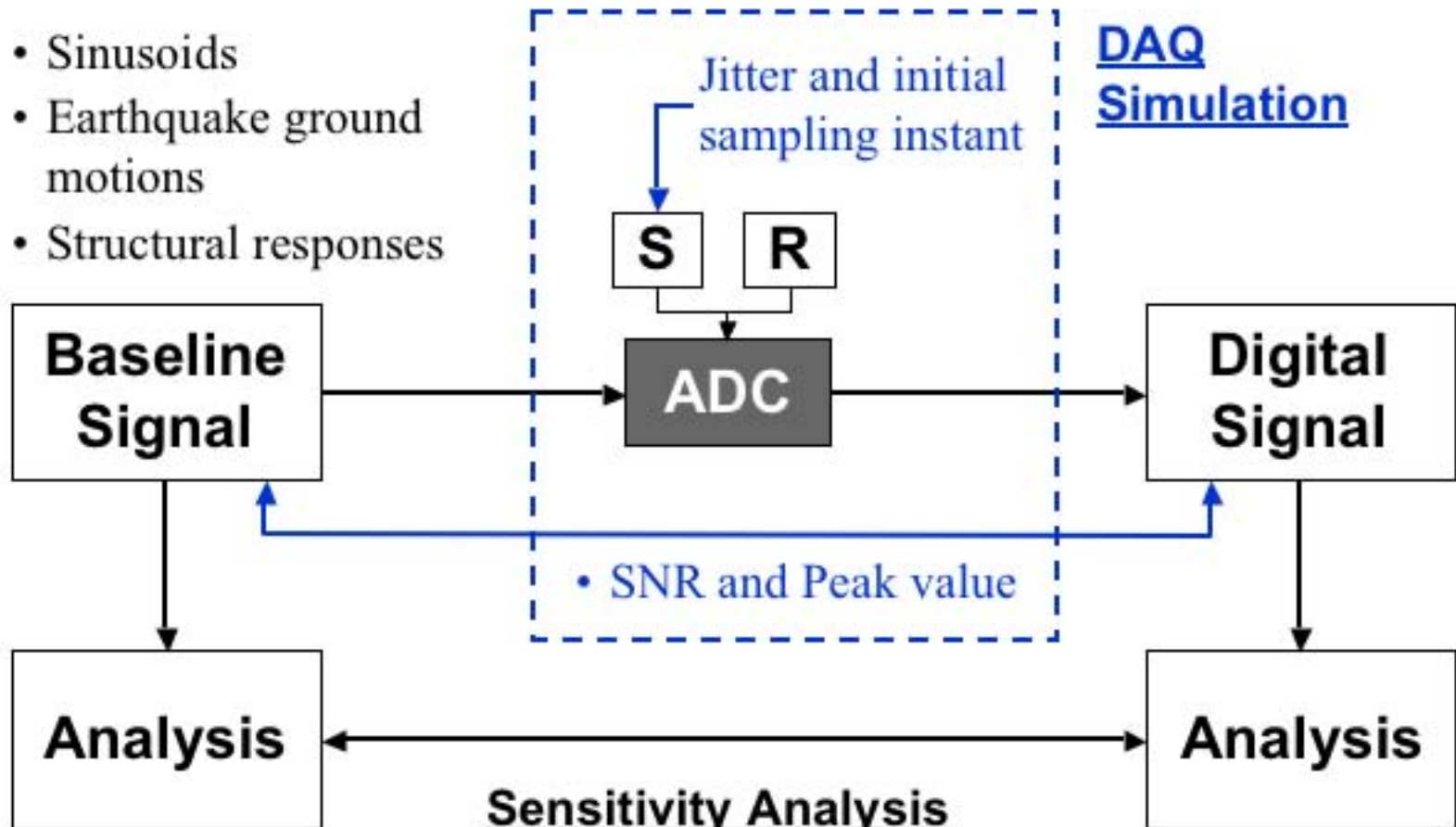


## Baseline Earthquake Record Set

- 30 EQ records downloaded from PEER, NCESMD, K-Net, KiK-Net, COSMOS
- Selected to capture broad nature of earthquakes
- Digitally enhanced to increase resolution: resample to 2kHz, zero-pads for filtering, band-pass filter 0.1-50Hz



- Sinusoids
- Earthquake ground motions
- Structural responses



## Clock Jitter

- Independent of sample rate
- Can be neglected

100sps

0.1 Hz  
1 Hz  
50 Hz

### Sinusoidal Signal

$$X(t) = A \sin[2\pi f t]$$

### Sampled Signal

$$x_i = A \sin[2\pi f t_i]$$

$$t_i = i \Delta t$$

### Jittery Sampled Signal

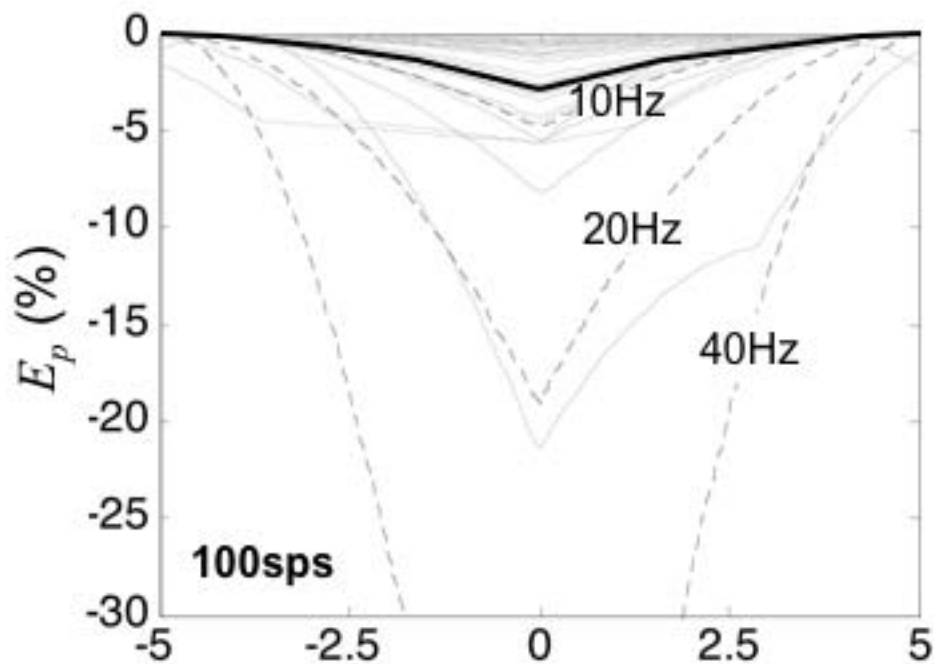
$$\bar{x}_i = A \sin[2\pi f \tau_i]$$

$$\tau_i \sim N(t_i, \sigma)$$

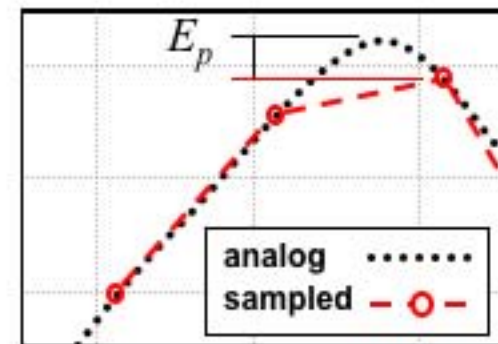


## Initial Sampling Instant

- Depends on sample rate
- Biased error – always negative



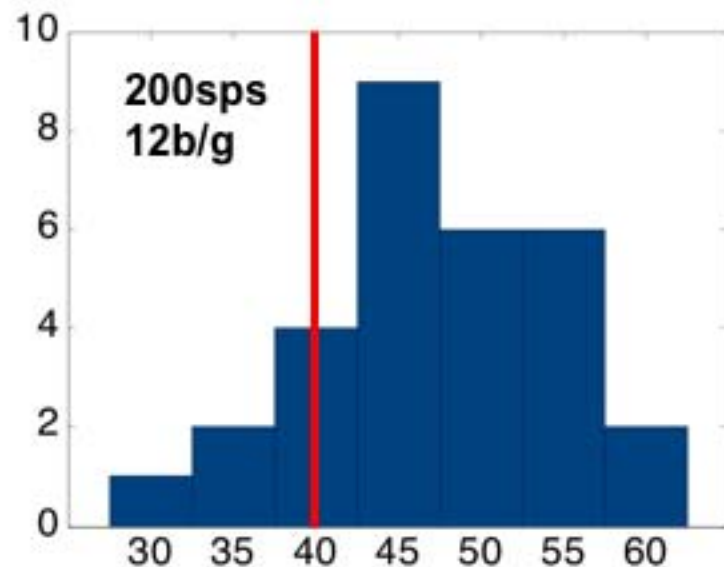
Error in peak value ( $E_p$ )



## X = EQ record

1.  $t_0 \sim U(0, \Delta t)$
2.  $t_i = t_0 + i \cdot \Delta t$
3.  $x_i = \text{interp}(X @ t_i)$
4.  $x_i = \text{round}(x_i / \text{res}) \cdot \text{res}$

- $S = [50-500]$  sps  $\rightarrow \Delta t = 1/S$
- $R = [6-24]$  bits/g  $\rightarrow \text{res} = g / 2^R$



## SNR

30

40dB

50dB

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## OBJECTIVE

Determine minimum requirements for specifications of sample rate, resolution, and time synchronization

## STRATEGY

Quantify the sensitivities of ground motion intensity measures and engineering response quantities to DAQ

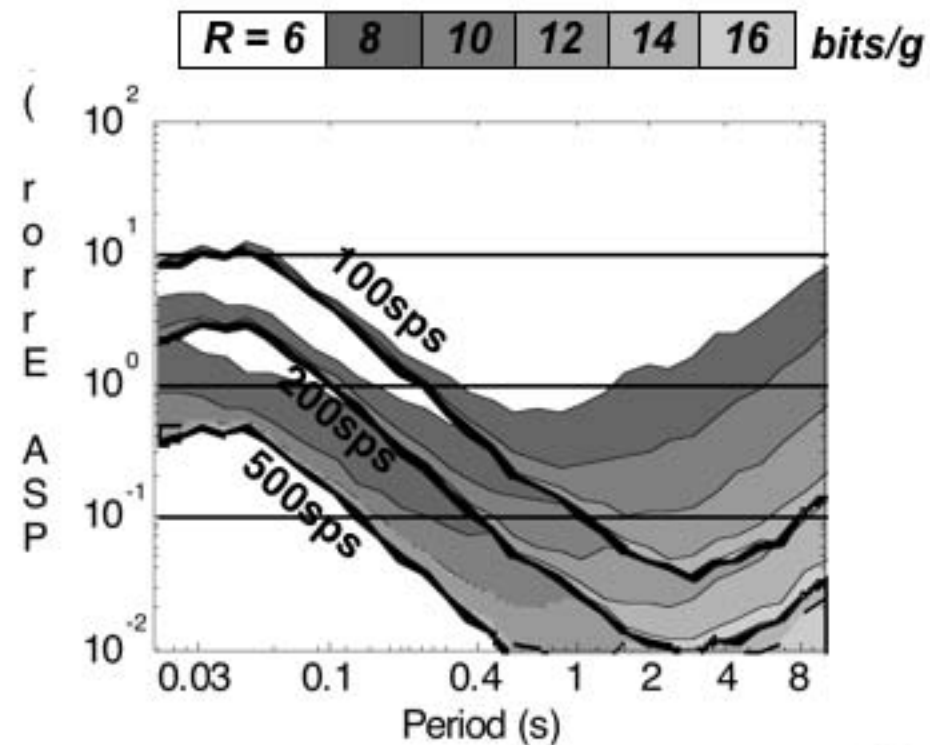
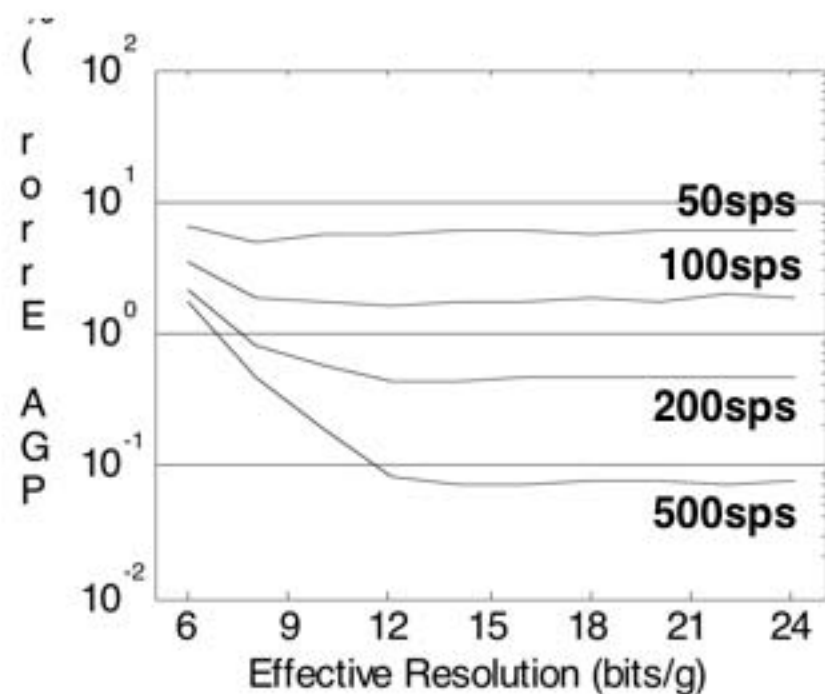
## APPROACH

1. Understand how engineers use strong-motion data
2. Simulate the *noisy* DAQ process
3. Perform sensitivity analyses

# SENSITIVITY ANALYSIS

## Intensity Measures

- PGA – 100sps, 6bits/g for error less than 5%
- PGV – 50sps, 8bits/g for error less than 5%
- PSA – 200sps, 8bits/g for error less than 5%

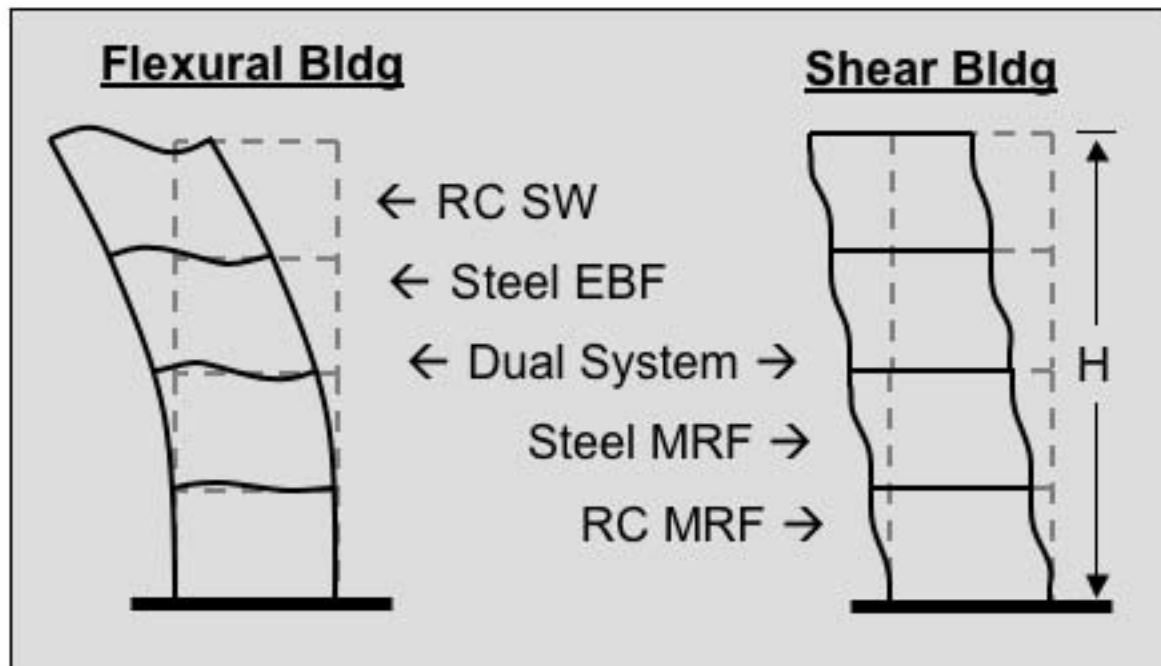




# SENSITIVITY ANALYSIS

## Baseline Building Response Set

- Simulate responses to baseline EQ record set by superimposed first few modal responses
- Assumptions: bounded by flexural & shear idealizations, uniform mass and stiffness,  $\zeta_n = 5\%$



$$\phi_n(x) = \sin \left[ \frac{2n-2}{2} \frac{\pi x}{H} \right]$$

$$T_n = \beta_n T_1$$

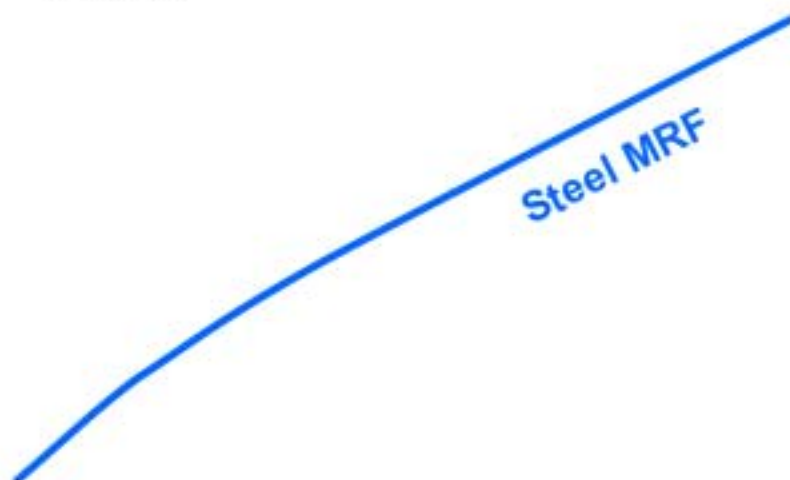
$$\Gamma_n = \frac{\int_0^H m \phi_n(x) dx}{\int_0^H m (\phi_n(x))^2 dx}$$

$$a_i = a_g + \sum_{n=1}^N \Gamma_n \phi_{ni} a_n$$

## Fundamental Period

- Depends on building structure and height... sort of
- Based on real data from instrumented buildings
- Empirical conventions in code (ASCE 7) are lower bounds

- Flexural
- Shear



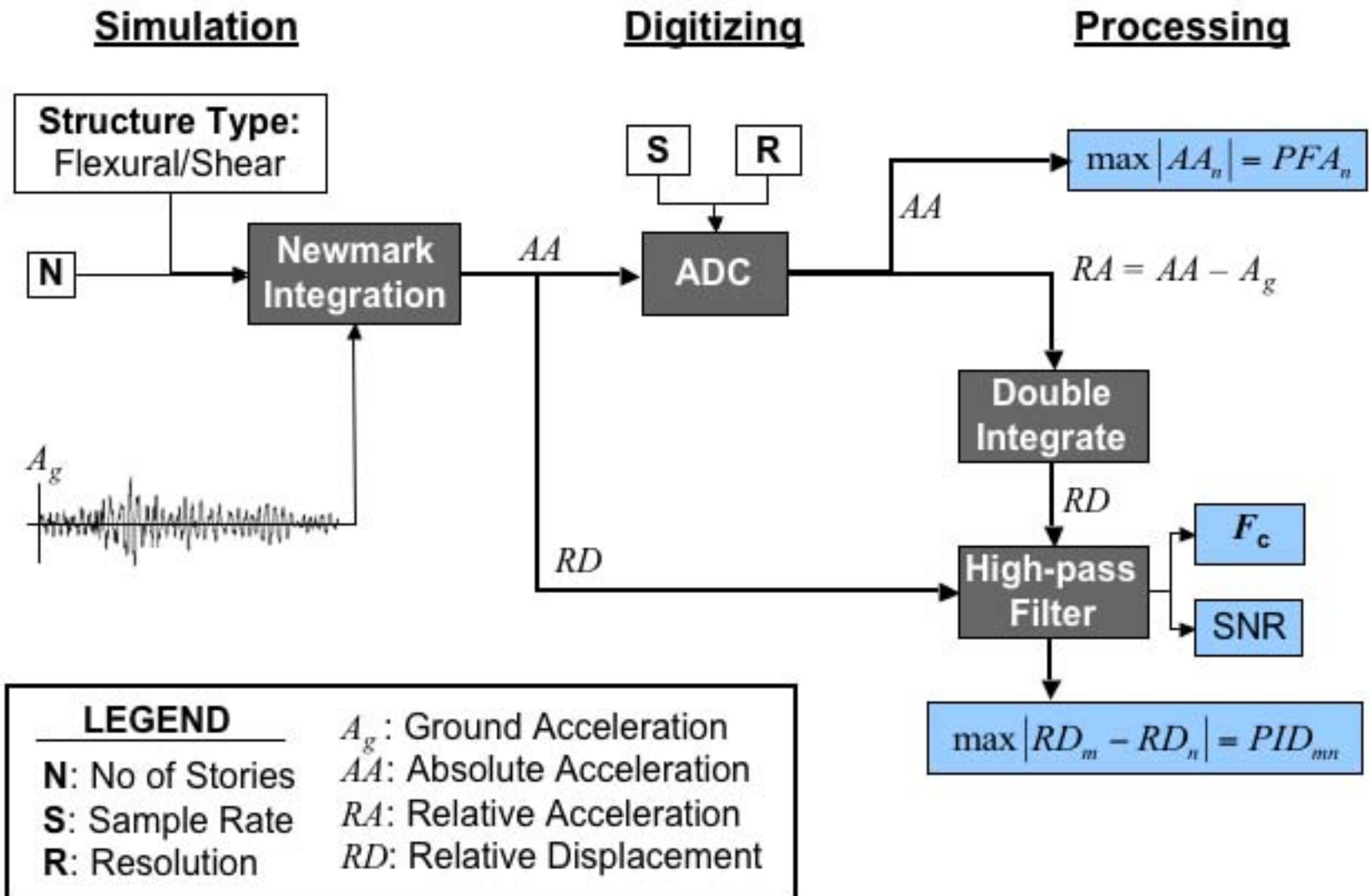
$$T_s = 0.68 + 0.11N$$

$$T_f = 0.46 + 0.03N$$

ASCE 7-05 S12.8.2.1

$$T_a = C_t h_n^x$$

# SENSITIVITY ANALYSIS



# SENSITIVITY ANALYSIS



No correction  
SNR = -31dB

Detrend  
SNR = -16.3dB

$F_c = 0.01\text{Hz}$   
SNR = -8.9dB

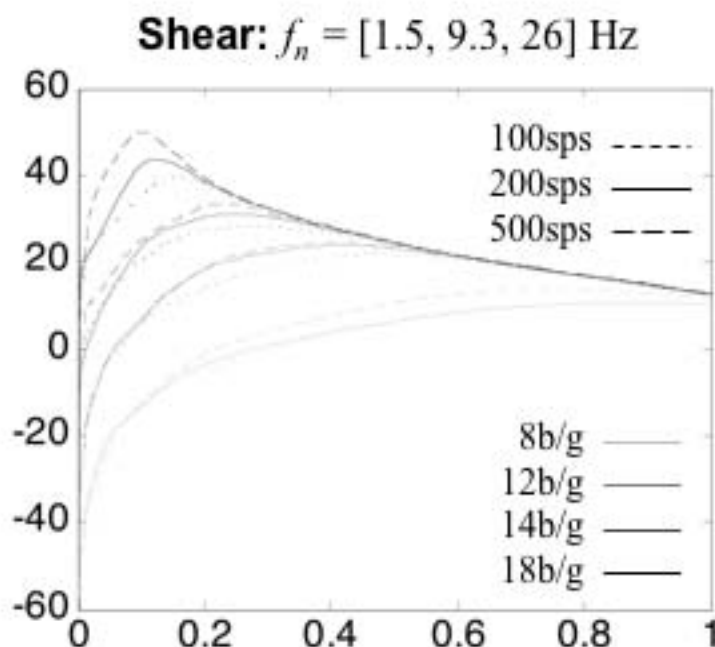
$F_c = 0.1\text{Hz}$   
SNR = 20.5dB

$F_c = 1.0\text{Hz}$   
SNR = 1.25dB

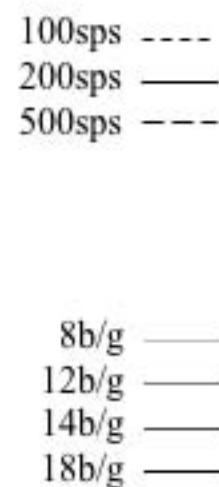
Displacement (in)

## Optimizing Frequency Cutoff

- High-pass 4<sup>th</sup> order acausal digital Butterworth filter
- A single floor of a 10-story bldg to one earthquake
- Resolution is important which corroborates Boore's (2003) findings of ADC quantization being a source of numerical drifts



**Flexural:**  $f_n = [0.4, 1.2, 1.9]$  Hz

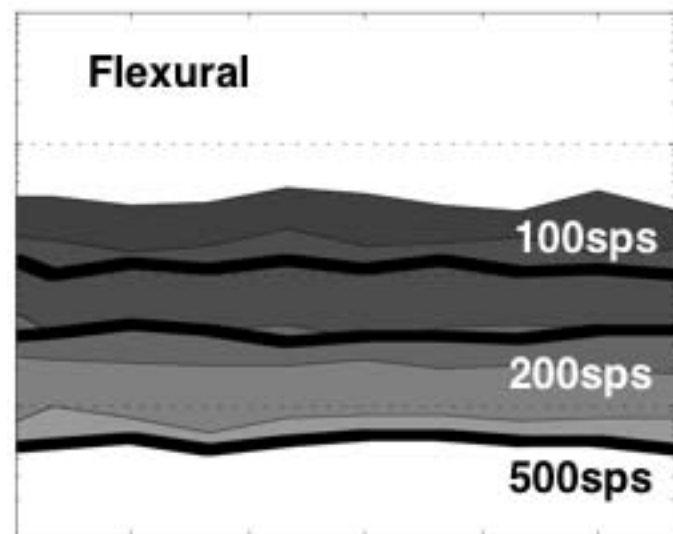




## Engineering Demand Parameters

- PFA – 100sps, 8b/g for error less than 5%
- PID – 100sps, 14b/g for error less than 5%

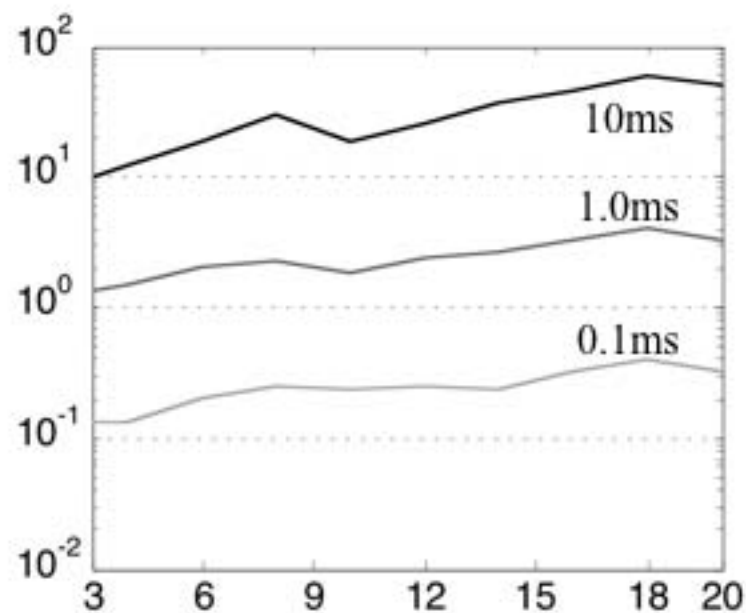
8 10 12 14 16 18 20 bits/g



Shear

## Time Synchronization Error

- Sync errors are additional to digitizing error
- PID – 200sps, 16b/g and sync to 1.0ms for total error < 5%



10ms

1.0ms

0.1ms

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<b>Specification</b>	<b>ANSS</b> (USGS 2005)	<b>CSMIP</b> (CGS 2007)	<b>Recommend</b> (Skolnik 2009)
Range	±4g	±4g	±4g
ADC Resolution	16bits	18bits	20bits
Sample Rate	200Hz	200Hz	200Hz
Sample Sync	0.05ms	0.2ms	1.0ms
Reference Time	1.0ms	0.5ms	

## Potential Improvements

- Other specifications – frequency response, dynamic range, cross-axis sensitivity, sensor layout
- Improved simulations – non-uniform stiffness; vary damping ratios, combo flex-shear shapes, non-linear responses
- Other engineering analyses – system identification

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Support provided by NSF CENS and nees@UCLA



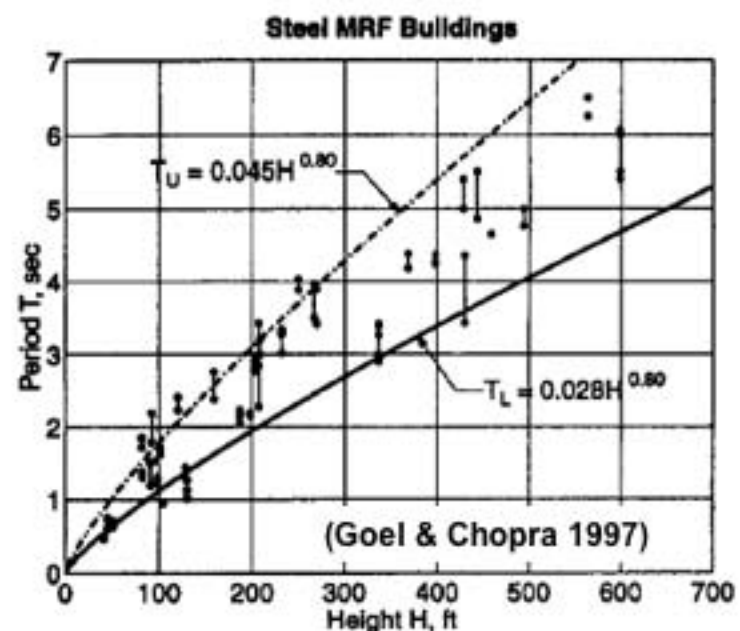
## Future Publications

BSSA: A quantitative basis for strong-motion instrumentation (12/09)

EQS: A quantitative basis for building instrumentation

## Engineering use of Strong-Motion Response Data

- Traditional – validate modeling assumptions and develop code provisions: fundamental period approximation formulas
- Modern – tall building issues, structural health monitoring (SHM)



## Tall Building Construction



One Rincon Hill - MKA

- Alternative designs citing Chap 16 of ASCE 7
- NDA of 3D FEM w/ suite of motions & peer review
- Exposed fundamental issues: ground motion selection, modeling guidelines, acceptance criteria
- LA-TBSDC publish document for LA-DBS (2008)
- Since 1965 LA requires accelerographs at base, mid-level, and roof
- UCLA, LA-DBS & CSMIP update requirements
- Deployment approval by peer review panel

Stories	Channels
10 – 20	15
20 – 30	21
30 – 50	24
> 50	30



## Structural Health Monitoring (SHM)

- Assess health of instrumented structures from measurements
- Detect damage before reaching critical state and allow for rapid post-event assessment
  - Potentially replacing expensive visual inspection which is impractical for wide spread damage in urban areas



## Strong Motion Instrumentation Programs (SMIP)

- CSMIP (CGS), ANSS & NSMP (USGS), K-net/KiK-net (Japan), Taiwan Seismology Center (CWB)
- Provide real-time ShakeMaps and data for engineers and scientists to improve hazard mitigation
- Since early 20<sup>th</sup> century with focus on ground monitoring
- Uniform structural instrumentation specifications are lacking



650 ground  
170 buildings



762 ground  
133 buildings



92 ground  
51 buildings

## Intensity Measures (IM)

- PGA – Peak Ground Acceleration
- PGV – Peak Ground Velocity
- PSA – Peak Response Spectral Pseudo-Acceleration
- MMI – Modified Mercalli Intensity

## Engineering Demand Parameters (EDP)

- PFA – Peak Floor Acceleration
- PID – Peak Interstory Drift

## Advanced Engineering Analyses

- SID – System Identification, Model Updating
- SHM – Structural Health Monitoring



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